

# Lecture #7 Force-Balanced MHD Equilibria

Hawes ①

## I. Review of MHD Equilibria

At Non-relativistic Eq:

$$\text{Force/Vol} = \rho \frac{\partial \underline{U}}{\partial t} + \rho \underline{U} \cdot \nabla \underline{U} = \underbrace{-\nabla p + \underline{j} \times \underline{B} - \rho \nabla \Phi_G}_{\text{Equilibrium has zero net force}} = 0$$

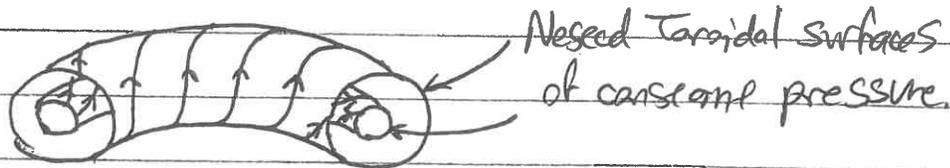
2. Neglecting gravity (generally valid for laboratory plasmas)

$$\nabla p = \underline{j} \times \underline{B} \quad \text{required for MHD Equilibrium}$$

- a. ZF  $\underline{j} \times \underline{B} = 0$  ( $|\nabla p| \ll |\underline{j} \times \underline{B}|$ ) Force-Free
- b. ZF  $\underline{j} \times \underline{B} \neq 0$  Force-Balanced

## 3. Hopf's Theorem:

a. A torus is simplest topological surface satisfying  $\nabla \cdot \underline{B} = 0$  &  $\underline{B} \cdot \nabla \alpha = 0$ .  
Thus, to contain a hot plasma, ~~the~~ magnetic field lines lie on closed surfaces of constant pressure:



## 4. Force-free Equilibrium Solutions

- a. Flux Ropes
- b. Reverse Field Pinch (RFP)

## II. Force-Balanced Equilibria:

A. Using Ampere's law, we may write force balance as

2. For  $p=p(x)$ ,  $\underline{B}=\underline{B}(x)$ , there exist an infinite number of solutions.

$$\nabla \left( p + \frac{B^2}{2\mu_0} \right) = \frac{(\underline{B} \cdot \nabla) \underline{B}}{\mu_0}$$

$\Rightarrow$  Let's focus on cylindrical and toroidal geometries

~~II. Pinch~~

### III. Force-Balanced Equilibria in Cylindrical Geometries

#### A. General Case:

1. We'll focus on the family of solutions with a magnetic field with no radial component and only radial dependence,

$$\underline{B} = B_\phi(r) \hat{\phi} + B_z(r) \hat{z} \quad (B_r = 0)$$

2. The radial component of the force balance (using NRL p. 6-7) gives

$$\frac{d}{dr} (p(r)) + \frac{[B_\phi(r)]^2}{2\mu_0} + \frac{[B_z(r)]^2}{2\mu_0} = - \frac{[B_\phi(r)]^2}{\mu_0 r}$$

NOTE: Magnetic tension term depends only on  $B_\phi$ .

3. Ampere's Law  $\underline{j} = \frac{1}{\mu_0} (\nabla \times \underline{B})$  gives

$$\underline{j} = -\frac{1}{\mu_0} \frac{dB_z}{dr} \hat{\phi} + \frac{1}{\mu_0 r} \frac{d}{dr} (r B_\phi) \hat{z}$$

4. Force balance depends on 3 functions

$p(r)$ ,  $B_\phi(r)$ ,  $B_z(r)$

- a. If two are given, the third is determined by force balance (solution to differential equation)

- b. We still have an infinite number of possible solutions  $\Rightarrow$  Certain limiting cases simplify the force balance equation.

#### B. The Z-Pinch:

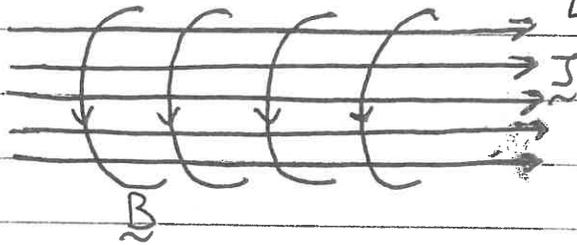
1. Here, we take  $B_z = 0$ . Therefore  $j_\phi = 0$ .

2.  $\frac{d}{dr} (p + \frac{B_\phi^2}{2\mu_0}) = - \frac{B_\phi^2}{\mu_0 r}$ 
  - a. The radial pressure gradient is entirely balanced by  $B_\phi$ .

- b.  $B_\phi$  is entirely generated by an axial current  $j_z$ .

III.  $B_0$  (Continued) The Z-Pinch

3.



Strong axial current through plasma produces a confining azimuthal  $B_\phi$ -field.

4. Consider a plasma of radius  $a$  with a constant axial current density inside the plasma,  $j_z = j_0$ .

a. Total Current:  $I_0 = \int_0^a \int_0^{2\pi} r dr d\phi j_0 = \pi a^2 j_0 \Rightarrow j_0 = \frac{I_0}{\pi a^2}$

b. Calculate the resulting  $B_\phi$  from Ampere's Law:

i)  $j_z = \frac{1}{\mu_0 r} \frac{d}{dr} (r B_\phi)$

ii)  $\int_0^r \frac{d}{dr} (r B_\phi) = r B_\phi = \int_0^r dr' \mu_0 r' j_z$  where  $j_z = \begin{cases} \frac{I_0}{\pi a^2} & r \leq a \\ 0 & r > a \end{cases}$

$$= \begin{cases} \int_0^r \frac{\mu_0 I_0}{\pi a^2} r' dr' & r \leq a \\ \int_0^a \frac{\mu_0 I_0}{\pi a^2} r' dr' & r > a \end{cases} = \begin{cases} \frac{\mu_0 I_0 r^2}{2\pi a^2} & r \leq a \\ \frac{\mu_0 I_0 a^2}{2\pi a^2} & r > a \end{cases}$$

iii) Thus  $B_\phi(r) = \begin{cases} \frac{\mu_0 I_0}{2\pi a^2} r & r \leq a \\ \frac{\mu_0 I_0}{2\pi r} & r > a \end{cases}$

c. Calculate the pressure  $p(r)$

i)  $\frac{dp}{dr} = -\frac{d}{dr} \left( \frac{B_\phi^2}{2\mu_0} \right) - \frac{B_\phi^2}{\mu_0 r} = \begin{cases} -\frac{2\mu_0 I_0^2 r}{4\pi^2 a^4} & r \leq a \\ 0 & r > a \end{cases}$

ii) At the edge of the plasma,  $r=a$ , we take  $p(a) = 0$ .

# Lecture # 7 (Continued)

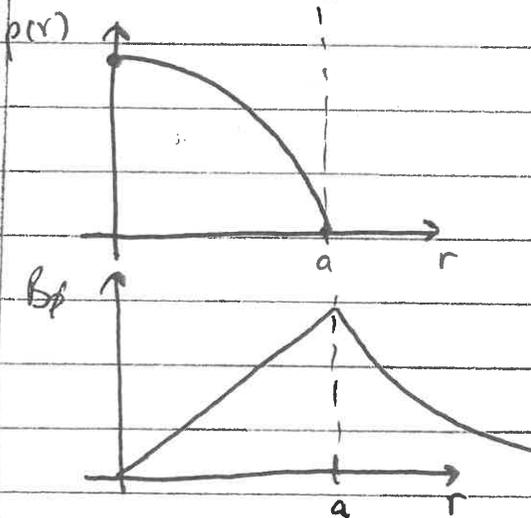
## III. B. 4. c. (Continued)

Hines ⊕

iii) Thus  $\int_r^a \frac{dp}{dr} r = p(a) - p(r) = \int_r^a \frac{2\mu_0 I_0^2 r}{4\pi^2 a^4} dr = -\frac{\mu_0 I_0^2}{4\pi^2 a^2} (1 - \frac{r^2}{a^2})$  By Boundary Conditions

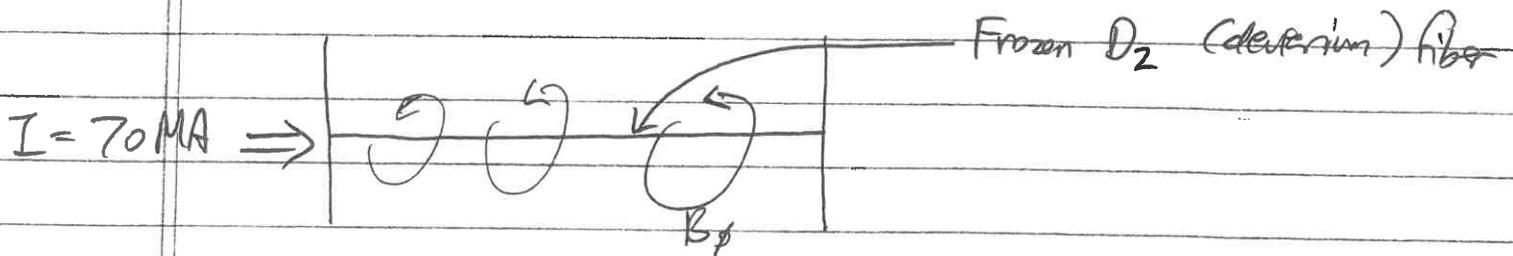
iv) Finally  $p(r) = \mu_0 \left(\frac{I_0}{2\pi a}\right)^2 \left(1 - \frac{r^2}{a^2}\right)$   $r \leq a$

### 5. Profiles of $p$ & $B_\theta$

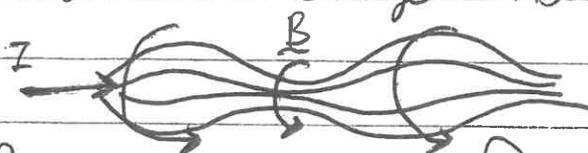


Magnetic pressure and magnetic tension confine thermal pressure.

### 6. The Z-Pinch at Sandia National Laboratories



- a. Enormous magnetic pressure (and tension) due to axial current confines plasma of MA deuterium in small volumes
- b. Unstable to "Sausage" instability



(Next semester we'll look at MHD Stability)

c. Produces copious x-rays from hot plasma. Useful for studies of high-energy-density plasmas!

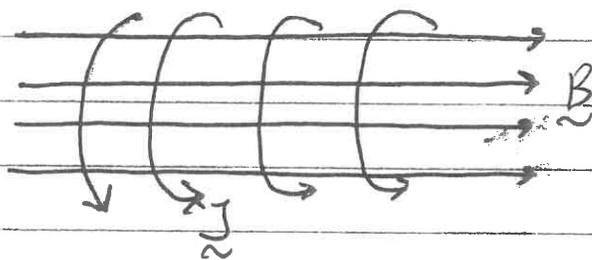
## Lecture # 7 (Continued)

HWes 5

### II. Continued

#### C. The "Therac" Pinch

1. In this case, we take  $B_\phi = 0$  and can solve for  $p(r)$  in terms of  $B_z(r)$ .

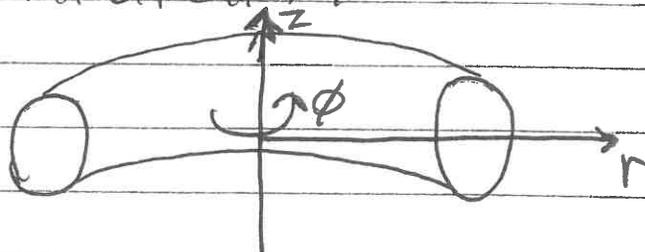


This is a homework problem!

Current in  $\phi$  direction produces  $B_z$  that confines pressure.

### III. Force-Balanced Equilibria in Toroidal Geometries

1. Although the cylindrical cases give us a good intuition of Force-Balanced MHD Equilibrium, it is toroidal geometries that are necessary to have confined in 3-D (Kippenhahn's theorem tells us the most at least have a torus).
2. We now consider toroidal geometries with symmetry in the toroidal direction  $\phi$ .



#### B. Magnetic Flux Coordinates:

1. For  $\frac{\partial}{\partial \phi} = 0$ ,  $\nabla \cdot \underline{B} = 0$  implies  $\frac{1}{r} \frac{\partial}{\partial r} (r B_r) + \frac{\partial B_z}{\partial z} = 0$ .
2. If we use the vector potential  $\underline{B} = \nabla \times \underline{A}$ , then  $\nabla \cdot \underline{B} = 0$  is automatically satisfied.

Lecture 7 (Continued)  
 III. B. (Continued)

Haves

3. The toroidal symmetry implies a simplification ( $\frac{\partial}{\partial \phi} = 0$ )

From NRL p.6

$$B_r = (\nabla \times \underline{A})_r = \frac{1}{r} \frac{\partial A_z}{\partial \phi} - \frac{\partial A_\phi}{\partial z} = -\frac{\partial A_\phi}{\partial z}$$

$$B_z = (\nabla \times \underline{A})_z = \frac{1}{r} \frac{\partial}{\partial r}(r A_\phi) - \frac{1}{r} \frac{\partial A_r}{\partial \phi} = \frac{1}{r} \frac{\partial}{\partial r}(r A_\phi)$$

4. Both  $B_r$  &  $B_z$  depend only on  $A_\phi$ !

4. Defining a flux function  $\psi(r, z) = r A_\phi$ , we get

$$B_r = -\frac{1}{r} \frac{\partial \psi}{\partial z}$$

$$B_z = \frac{1}{r} \frac{\partial \psi}{\partial r}$$

5. NOTE: For  $\psi(r, z)$ ,  $\underline{B} \cdot \nabla \psi = B_r \frac{\partial \psi}{\partial r} + B_z \frac{\partial \psi}{\partial z} = B_r(B_z r) + B_z(-B_r r) = 0$

a. Thus, ~~the magnetic field lines are~~  $\underline{B} \cdot \nabla \psi = 0$

Magnetic field lines must lie on surfaces of  $\psi = \text{const.}$

b. But, we also know ~~the magnetic field lines are~~  $\underline{B} \cdot \nabla p = 0$

from the force balance, so  $p = p(\psi)$

6. Consider the  $\phi$ -component of  $\underline{j} \times \underline{B} = \nabla p$ :

a.  $j_z B_r - j_r B_z = \frac{1}{r} \frac{\partial p}{\partial \phi}$  but  $\frac{1}{r} \frac{\partial p(\psi)}{\partial \phi} = 0$  since  $\psi = \psi(r, z)$ .

NRL p.6

b. Ampere's Law gives:  $j_r = \frac{1}{\mu_0} (\nabla \times \underline{B})_r = \frac{1}{\mu_0} \left[ \frac{1}{r} \frac{\partial B_z}{\partial \phi} - \frac{\partial B_\phi}{\partial z} \right]$

$$j_z = \frac{1}{\mu_0} (\nabla \times \underline{B})_z = \frac{1}{\mu_0} \left[ \frac{1}{r} \frac{\partial}{\partial r}(r B_\phi) - \frac{1}{r} \frac{\partial A_r}{\partial \phi} \right]$$

As with  $B_j$  in terms of  $\underline{A}$ ,  $\underline{j}$  depends only on  $B_\phi(r, z)$ .

c. Analogous, we define a second flux function  $F = r B_\phi$  so  
 such that  $j_z B_r - j_r B_z = 0$ .

Lecture # 7 (Continued)  
 III. B. G. (Continued)

Howes (7)

d. It follows that  $B_r \frac{\partial F}{\partial r} + B_z \frac{\partial F}{\partial z} = 0 \Rightarrow \underline{B} \cdot \nabla F = 0$

and so  $\boxed{F = F(\psi)}$

7. Thus, we can express the toroidally symmetric magnetic field in terms of two scalar Flux Functions  $\psi(r, z), F(r, z)$ .

a.  $\underline{B} = \left(-\frac{1}{r} \frac{\partial \psi}{\partial z}\right) \hat{r} + \left(\frac{1}{r} \frac{\partial \psi}{\partial r}\right) \hat{z} + \left(\frac{F(\psi)}{r}\right) \hat{\phi}$

Magnetic field expressed using Magnetic Flux Coordinates

b. This can also be expressed  $\underline{B} = \frac{\nabla \psi}{r} \times \hat{\phi} + \frac{F(\psi)}{r} \hat{\phi}$

C. The Grad-Shafranov Equation:

1. Now, let's consider the r-component of the force balance.

$$j_\phi B_z - j_z B_\phi = \frac{\partial p}{\partial r}$$

2. First use Ampere's Law to calculate  $j_\phi$

$\mu_0 j_\phi = (\nabla \times \underline{B})_\phi = \frac{\partial B_r}{\partial z} - \frac{\partial B_z}{\partial r} = -\frac{1}{r} \frac{\partial^2 \psi}{\partial z^2} - \frac{\partial}{\partial r} \left(\frac{1}{r} \frac{\partial \psi}{\partial r}\right) = -\frac{1}{r} \Delta^* \psi$

$$B_r = -\frac{1}{r} \frac{\partial \psi}{\partial z}, \quad B_z = \frac{1}{r} \frac{\partial \psi}{\partial r}$$

3. Similarly

$\mu_0 j_z = (\nabla \times \underline{B})_z = \frac{1}{r} \frac{\partial}{\partial r} (r B_\phi) - \frac{1}{r} \frac{\partial B_r}{\partial \phi} = \frac{1}{r} \frac{\partial F}{\partial r}$   
 $F = r B_\phi$

4. Thus  $-\frac{1}{r} \Delta^* \psi B_z - \frac{1}{r} \frac{\partial F}{\partial r} B_\phi = \mu_0 \frac{\partial p}{\partial r}$

a. Again, substituting for  $B_z$  &  $B_\phi$  gives

$$-\frac{1}{r} \Delta^* \psi \left(\frac{1}{r} \frac{\partial \psi}{\partial r}\right) - \frac{1}{r} \frac{\partial F}{\partial r} \left(\frac{F}{r}\right) = \mu_0 \frac{\partial p}{\partial r}$$

# Lecture #7 (Continued)

Hines (8)

## III. C. (Continued)

5. NOTE:  $F = F(\psi)$  and  $p = p(\psi)$ , so

$$\frac{\partial F^2}{\partial r} = \frac{dF^2}{d\psi} \frac{\partial \psi}{\partial r} \quad \text{and} \quad \frac{\partial p}{\partial r} = \frac{dp}{d\psi} \frac{\partial \psi}{\partial r}$$

Thus

$$-\frac{1}{r^2} \Delta^* \psi \left( \frac{\partial \psi}{\partial r} \right) - \frac{1}{2r^2} \frac{dF^2}{d\psi} \left( \frac{\partial \psi}{\partial r} \right) = \mu_0 \frac{dp}{d\psi} \left( \frac{\partial \psi}{\partial r} \right)$$

6. Finally, we obtain

$$\Delta^* \psi = -\mu_0 r^2 \frac{dp}{d\psi} - \frac{1}{2} \frac{dF^2}{d\psi}$$

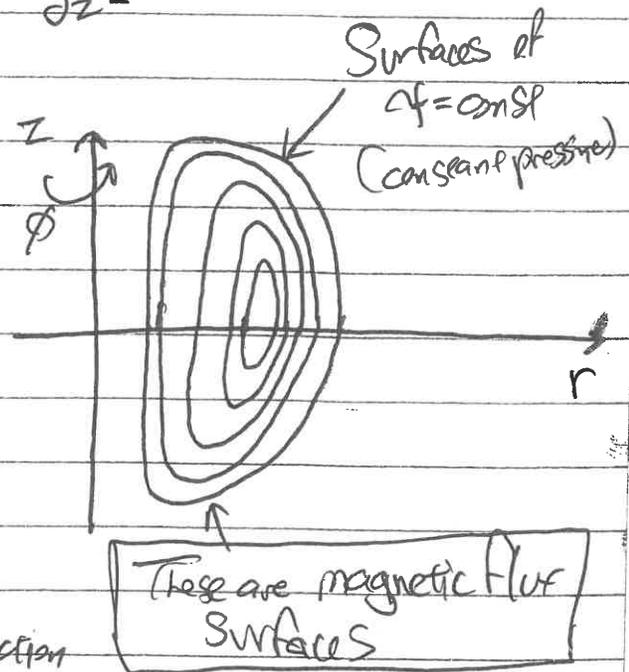
Grad-Shafranov Equation

where  $\Delta^* \psi \equiv r \frac{\partial}{\partial r} \left( \frac{1}{r} \frac{\partial \psi}{\partial r} \right) + \frac{\partial^2 \psi}{\partial z^2}$

## D. Application

1. Grad-Shafranov equations is used to calculate

Magnetostatic Equilibria  
in axisymmetric toroidal systems,



2. In practice:

a. Specify  $p(\psi)$  and  $F(\psi)$   
 Pressure  $\nearrow$   $\nwarrow$  Toroidal Field Function

b. Solve Grad-Shafranov Eq (Numerically) with specified boundary conditions for  $\psi(r, z)$

c. Pressure profile is then determined  $p = p(\psi(r, z))$

3. Exact analytical solutions, known as Solov'ev equilibria, are often used in analysis of toroidal magnetic fusion devices.