

# Lecture #18

Ref: Burgess & Scholer, Collisionless Shocks in Space Plasmas, Cambridge (2015)

## I. MHD Shock Geometry!

### A. Earth's Bow Shock

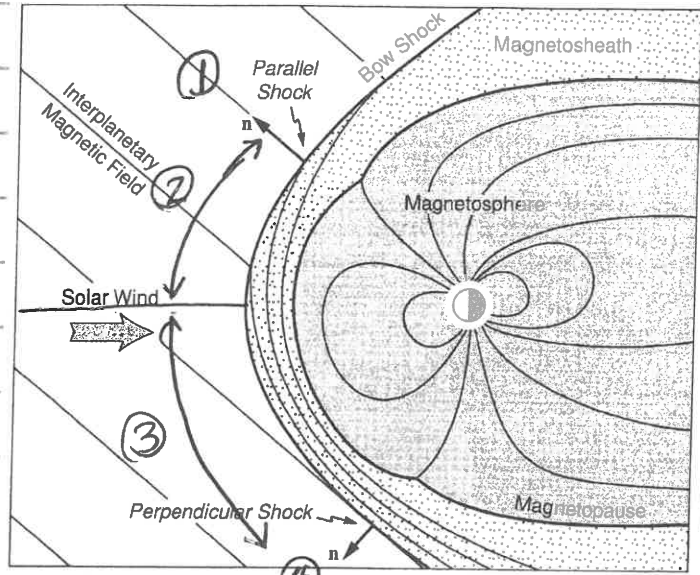
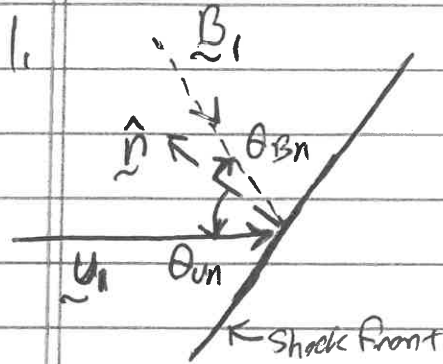


Fig. 8.10. Parallel and perpendicular bow shock regions.

### 2. Def: Shock Normal

$\hat{n}$  - direction perpendicular to shock surface.

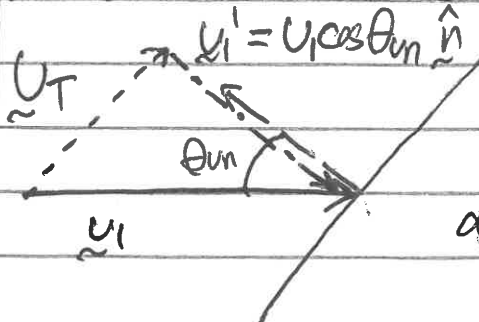
### 3. Def: Shock normal angle of magnetic field, $\theta_{Bn}$

### b Def: Shock normal angle of upstream flow, $\theta_{un}$

### 4. Def: Normal Incidence Frame (NIF)

a. Frame of reference in which upstream flow is parallel to the normal.

b. We are free to change to NIF frame.



$$\begin{aligned}
 & \left. \begin{aligned}
 \text{a. } \underline{u}'_i = \underline{u}_i + \underline{u}_T = u_1 \cos \theta_{un} \hat{n} \\
 \text{d. } \underline{u}_T = \underline{u}_i - u_1 \cos \theta_{un} \hat{n}
 \end{aligned} \right\} \underline{u}'_i \parallel \hat{n}
 \end{aligned}$$

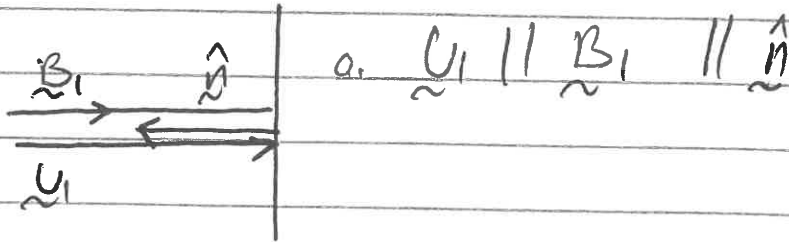
# I.A. 4. (Continued)

Haves 2

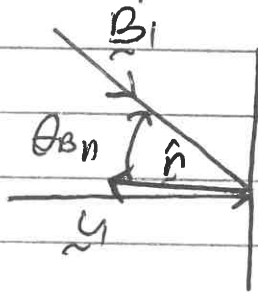
e. In the NIF,  $\theta_{bn}$  is eliminated as a parameter.

## B. Shock-Normal Angle Ranges: (NIF frame)

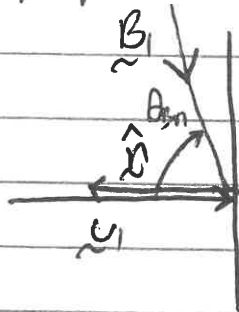
① Parallel Shock:  $\theta_{bn} = 0^\circ$



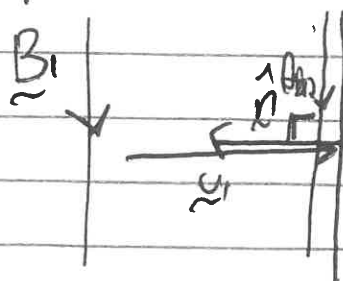
② Quasi-parallel Shock  $0^\circ < \theta_{bn} \leq 45^\circ$



③ Quasi-perpendicular Shock  $45^\circ \leq \theta_{bn} < 90^\circ$



④ Perpendicular Shock  $\theta_{bn} = 90^\circ$



B. MHD Shock Parameters

1. For a stationary Bow shock at the Earth, the shock will be determined by the upstream flow parameters.

$$P_1, \rho_1, \underline{B}_1, \underline{u}_1$$

subscript "1" - upstream  
"2" - downstream

2. Transforming frame to NIF  $\underline{u}_1 \rightarrow \underline{u}_n$  (eliminate  $\underline{u}_n$ )

3. Due to coplanarity theorem  $\underline{B}_1$  and  $\underline{B}_2$  lie in the same plane (for compressive shocks), so we can use  $B_1 = |\underline{B}_1|$  and  $\theta_{Bn}$  to parameterize.

4. In the NIF, MHD shocks can be characterized by three dimensionless parameters.

a. Upstream Alfvén Mach number:  $M_A \equiv \frac{u_1}{v_{A1}}$

where  $v_{A1} = \frac{B_1}{\sqrt{\mu_0 \rho_1}}$

b. Upstream Plasma Beta:  $\beta_1 = \frac{2\mu_0 n_1 k T_1}{B_1^2} = \frac{2\mu_0 P_1}{B_1^2}$

(Ratio of thermal pressure  $p_1 = n_1 k T_1$  to mag press  $P_{B1} = \frac{B_1^2}{2\mu_0}$ )

c. Shock-normal angle  $\theta_{Bn}$

5. Recall, for linear MHD waves,  $\omega = \omega(\beta_1, \theta_{Bn})$

## C. Solutions of MHD Rankine-Hugoniot Jump Conditions

1. Def: Shock Compression Ratio  $r \equiv \frac{\rho_2}{\rho_1}$

2. We can define all of the jumps in terms of  $M_A, \beta_1, \theta_{Bn}$ .  
a. below, we assume monatomic plasma,  $\gamma = 5/3$

3. Compression,  $r$ :

$$\textcircled{A} \quad \cos^2 \theta_{Bn} (2M_A^2 + 5\beta_1 \cos^2 \theta_{Bn}) r^3 + M_A^2 \{ M_A^2 - \cos^2 \theta_{Bn} (5M_A^2 + 8 + 10\beta_1) \} r^2 + M_A^4 (11 \cos^2 \theta_{Bn} + 2M_A^2 + 5 + 5\beta_1) r - 8M_A^6 = 0$$

4. Transverse Magnetic Field,  $B_{t2}$

$$\textcircled{B} \quad \frac{B_{t2}}{B_{t1}} = \frac{r(M_A^2 - \cos^2 \theta_{Bn})}{(M_A^2 - r \cos^2 \theta_{Bn})}$$

5. Transverse Velocity,  $U_{t2}$

$$\textcircled{C} \quad \frac{U_{t2}}{U_1} = \frac{\sin \theta_{Bn} \cos \theta_{Bn} (r-1)}{(M_A^2 - r \cos^2 \theta_{Bn})}$$

6. Downstream Pressure  $p_2$

$$\textcircled{D} \quad \frac{p_2}{(\rho_1 U_1^2)} = \frac{15}{2} \left\{ \frac{\beta_1}{M_A^2} + \frac{2(r-1)}{r} + \frac{\sin^2 \theta_{Bn}}{M_A^2} \left[ 1 - \left( \frac{B_{t2}}{B_{t1}} \right)^2 \right] \right\}$$

7. NOTE:  $p = nkT \Rightarrow p = \rho \frac{kT}{m} \Rightarrow \boxed{\frac{kT}{m} = \frac{p}{\rho}}$

a. Can be used to convert  $p_2$  to  $T_2$  given  $\rho_2$ .

8. Coplanarity and downstream tangential velocity

a. In the NIF, upstream  $\boxed{u_{t1} = 0}$

b. Magnetic tension (due to bending of  $\underline{B}$  at the shock discontinuity) can impart an impulse that generates  $u_{t2} \neq 0$ . This is distinct from hydrodynamic shocks.

c. There is no magnetic tension force perpendicular to the magnetic coplanarity plane.

d. Thus,  $u_{t2} \neq 0$  must lie in the same coplanarity plane containing  $\underline{B}_{t1}$  and  $\underline{B}_{t2}$ !

e. NOTE: Within the shock transition, there may be components of  $\underline{u}_t$  and  $\underline{B}_t$  not within the coplanarity plane. But, downstream  $\underline{u}_{t2}$  and  $\underline{B}_{t2}$  will lie in the coplanarity plane.

D. Strong Shock Limit:  $M_A \gg 1$

1. In this limit  $M_A \gg 1$ , (A) reduces to

$$2r \frac{M_A^6}{A} - 8 \frac{M_A^6}{A} = 0 \Rightarrow \boxed{r = \frac{p_2}{p_1} = 4}$$

I. D. (Continued)

Howes (6)

2. Transverse magnetic field jump  $\text{B} \cdot \hat{n}$ :  $\frac{B_{t2}}{B_{t1}} = \frac{r(M_A^2 - \cos^2 \theta_{Bn})}{(M_A^2 - r \cos^2 \theta_{Bn})}$

b.  $\frac{B_{t2}}{B_{t1}} = r = 4$

3. Pressure  $\text{D}$ : a.  $\frac{p_2}{(\frac{1}{2} \rho_1 u_1^2)} = \frac{1}{2} \frac{2(r-1)}{r} = \frac{4-1}{4} = \frac{3}{4}$

b. Thus  $p_2 \approx \frac{3}{4} (\frac{1}{2} \rho_1 u_1^2)$  Downstream pressure jump is unlimited

c. NOTE: Pressure and energy density have the same units

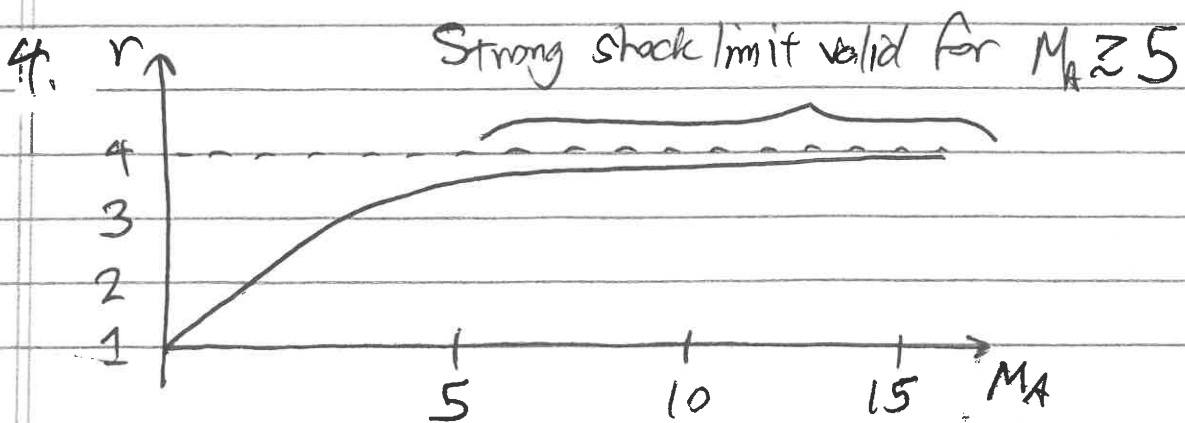
$$[P] = \frac{N}{m^2} \quad [\frac{1}{2} \rho_1 u_1^2] = \frac{J}{m^3} = \frac{N \cdot m}{m^3} = \frac{N}{m^2} \checkmark$$

d. For a strong shock with  $u_2 \rightarrow \frac{1}{4} u_1$ , (since  $r = \frac{\rho_2}{\rho_1} = \frac{u_1}{u_2}$ ) what is the change in kinetic energy of the flow?

i)  $\frac{1}{2} \rho_1 u_1^2 - \frac{1}{2} \rho_2 u_2^2 = \frac{1}{2} \underbrace{\rho_0}_{\text{constant}} (u_1 - u_2) = \frac{1}{2} \rho_0 (u_1 - \frac{u_1}{4}) = \frac{3}{4} (\frac{1}{2} \rho_0 u_1^2)$

ii) Thus, the loss incoming kinetic energy of the flow is converted to thermal energy!

Upstream kinetic energy  $\Rightarrow$  downstream thermal energy!





I. (Continued)

Pages 7

F. Perpendicular Shock Limit:  $\theta_{sn} = 90^\circ$

1. Setting  $\cos \theta_{sn} = 0$ , (A) reduces to a quad eqn

$$a. \quad r^2 + 2r \left[ M_A^2 + \frac{5}{2}(1 + \beta_1) \right] - 8 M_A^2 = 0$$

$$b. \quad r = - \left[ M_A^2 + \frac{5}{2}(1 + \beta_1) \right] \pm \sqrt{\left[ M_A^2 + \frac{5}{2}(1 + \beta_1) \right]^2 + 8 M_A^2}$$

↑  
Since  $r > 0$  for a shock, only take (+) sign!

2. Alfvén Mach number threshold for a perpendicular shock:

a. A shock occurs when  $r > 1$ , so one may set  $r = 1$  and solve for  $M_A$  to determine the threshold for a shock.

$$b. \quad 1 = - \underbrace{\left[ M_A^2 + \frac{5}{2}(1 + \beta_1) \right]}_{=A} + \sqrt{\underbrace{\left[ M_A^2 + \frac{5}{2}(1 + \beta_1) \right]^2 + 8 M_A^2}_{=A}}$$

$$c. \quad (1 + A)^2 = A^2 + 8 M_A^2$$
$$1 + 2A + A^2 = A^2 + 8 M_A^2$$
$$1 + 2 M_A^2 + 5(1 + \beta_1) = 8 M_A^2$$
$$6 + 5\beta_1 = 6 M_A^2$$
$$1 + \frac{5}{6}\beta_1 = M_A^2$$

d. Note:  $M_A^2 = \frac{U_1^2}{V_A^2}$ , so  $U_1^2 = V_A^2 + \frac{5}{6}\beta_1 V_A^2$

$$i) \quad \frac{5}{6}\beta_1 V_A^2 = \frac{5}{6} \frac{2\mu_0 \rho_1}{\beta_1^2} \frac{\beta_1^2}{\mu_0 \rho_1} = \frac{5}{3} \frac{\rho_1}{\rho_1} = \boxed{\frac{\partial \rho_1}{\rho_1} = c_s^2}$$

$$ii) \quad \text{Thus } U_1^2 = V_A^2 + c_s^2$$

e. Thus, threshold is  $\frac{U_1^2}{V_A^2 + c_s^2} = 1$

f. For  $\theta_{Bn} = 90^\circ$ , the fast magnetosonic speed is

$$V_f^2 = V_A^2 + c_s^2 \quad \text{for } \theta_{Bn} = 90^\circ$$

g. Define: Fast Magnetosonic Mach Number, (Perpendicular shock)  $M_f = \frac{U_1}{V_f}$

h. Fast Magnetosonic Shock occurs when  $M_f > 1$

F. Parallel Shock Limit:  $\theta_{Bn} = 0^\circ$

1. Seeing as  $\theta_{Bn} = 1$ , (A) can be factored to obtain three roots for  $r$ .

2. The magnetosonic root (which depends on  $\beta_1$ ) yields a threshold upstream flow of

$$U_1 = c_s$$

a. Define: Sonic Mach Number  $M = \frac{U_1}{c_s}$

$$\text{where } c_s^2 = \frac{\delta p_1}{\rho_1}$$

b. Parallel Shock occurs when  $M > 1$

c. This is equivalent to a hydrodynamic shock (see Lec #15).

i) Magnetic field drops out

ii) Parallel MHD Shock is purely hydrodynamic.



G. Oblique Shocks:  $0^\circ < \theta_{Bn} < 90^\circ$

1. For oblique shocks, (A) has three different roots for  $r$ :

- a. Fast magnetosonic Shock
- b. Slow magnetosonic Shock
- c. Intermediate (Alfvénic) Shock

2. To determine the threshold inflow speed for each root, set  $r=1$ , and (A) can be factored to

$$\underbrace{(M_A^2 - \cos^2 \theta_{Bn})}_{\text{Intermediate Shock}} \underbrace{\left\{ M_A^4 - M_A^2 \left( 1 + \frac{5}{6} \beta \right) + \frac{5}{6} \beta \cos^2 \theta_{Bn} \right\}}_{\text{Fast \& Slow Shocks}} = 0$$

a. MHD Wave Speeds:

$$\left. \begin{matrix} v_F \\ v_S \end{matrix} \right\} = \left\{ \frac{1}{2} \left[ v_A^2 + c_s^2 \pm \sqrt{(v_A^2 + c_s^2)^2 - 4v_A^2 c_s^2 \cos^2 \theta_{Bn}} \right] \right\}^{\frac{1}{2}}$$

Fast (top) / Slow (bottom)

Comp velocity of Alfvén wave along  $\hat{n}$

$$v_{GA} = v_A \cos \theta_{Bn}$$

Alfvén speed (constant)

$$v_A^2 = \frac{B_1^2}{\mu_0 \rho_1}$$

Sound speed

$$c_s^2 = \frac{\gamma p_1}{\rho_1}$$

b.  $M_F = \frac{v_1}{v_F}$

c.  $M_S = \frac{v_1}{v_S}$

d.  $M_A = \frac{v_1}{v_A}$

Formally,  $v_F$  &  $v_S$  depend on  $\theta_{Bn}$  (and  $\beta$ )

NOTE: Since it is difficult observationally to determine  $\theta_{Bn}$ ,  $M_A$  is defined relative to the (total) Alfvén velocity.

## 3. Slow vs. Fast Magnetosonic Shocks:

a. A slow shock will form if  $M_s > 1$  but  $M_f < 1$

b. This is a narrow range of upstream velocities,

c. For heliospheric shocks, typically  $M_f > 1$ , so we usually see only fast magnetosonic shocks.

e.g. Earth's bow shock:  $M_A \sim 10 \Rightarrow M_f \gtrsim 3$ .  
For typically  $\beta_1$  values.

Reference:

D. Burgess & M. Scholer, "Collisionless Shocks in Space Plasmas: Structure and Accelerated Particles", Cambridge University Press, 2015.