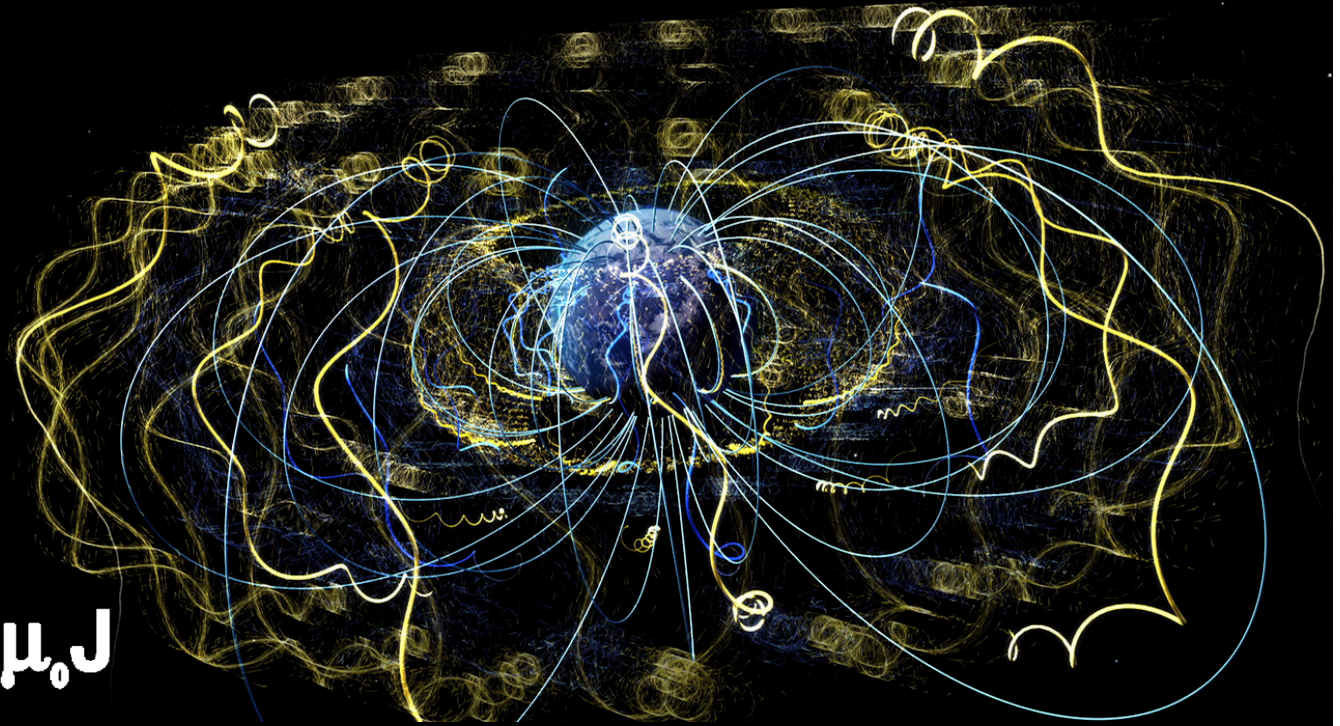


$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon_0}$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{B} = \mu_0 \epsilon_0 \frac{\partial \mathbf{E}}{\partial t} + \mu_0 \mathbf{J}$$



Electricity and Magnetism II: 3812

Professor Jasper Halekas
Van Allen 70
MWF 9:30-10:20 Lecture

Boundary Conditions

Interface w/ no free charge
or current

$$\Delta D_{\perp} = \Delta(\epsilon E_{\perp}) = 0$$

$$\Delta \vec{E}_{\parallel} = 0$$

$$\Delta \theta_{\perp} = 0$$

$$\Delta \vec{H}_{\parallel} = \Delta(\vec{B}_{\parallel}/\mu) = 0$$

Normal Incidence

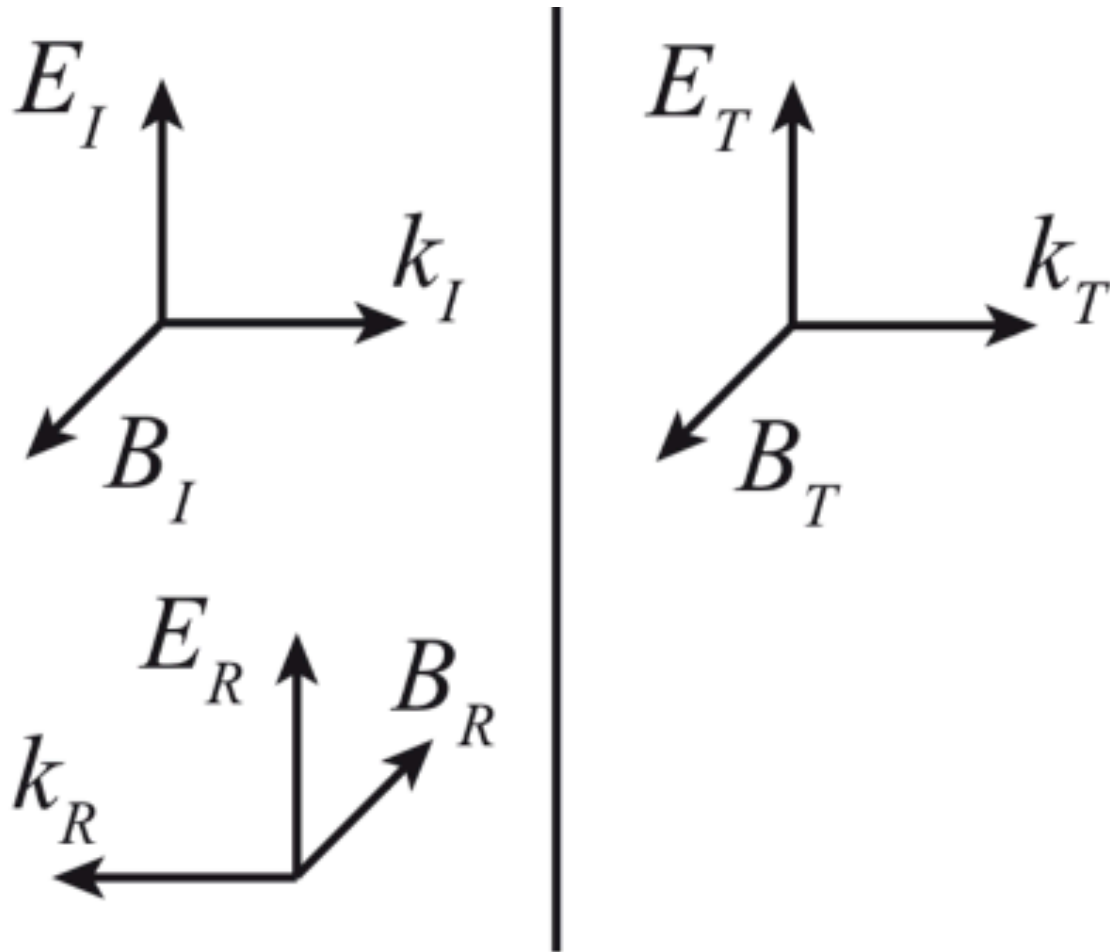
- Boundary at $x-y$ plane ($z=0$)
- Pick $\vec{k} = k \hat{z}$, $\hat{n} = \hat{x}$
- $\vec{E}, \vec{B} \perp \vec{k}$ so $E_{\perp} = B_{\perp} = 0$

Incident:
$$\vec{E}_I(z,t) = \vec{E}_{0I} e^{i(k_1 z - \omega t)} \hat{x}$$
$$\vec{B}_I(z,t) = \frac{\vec{E}_{0I}}{v_1} e^{i(k_1 z - \omega t)} \hat{y}$$

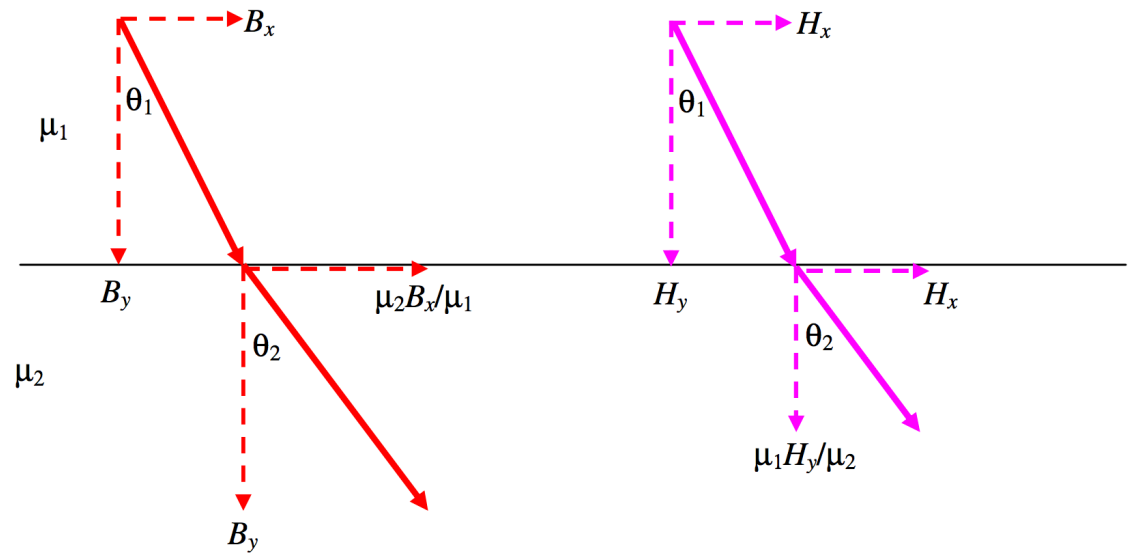
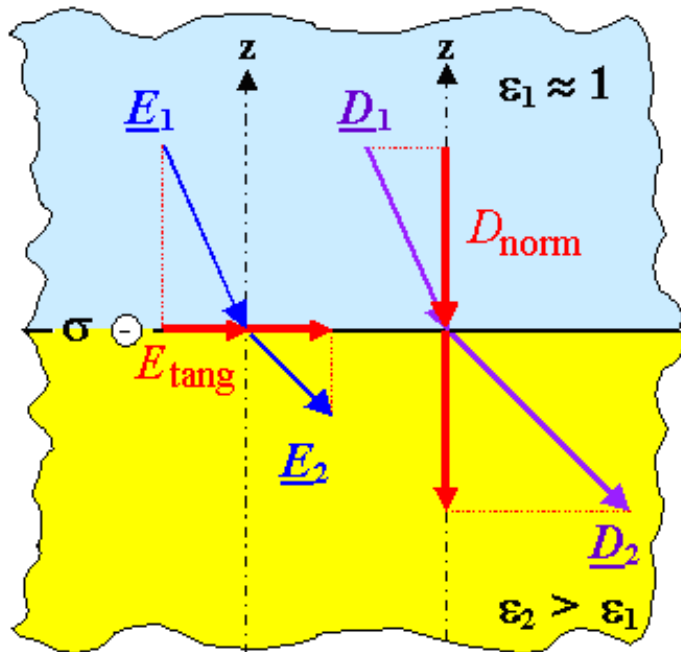
Reflected:
$$\vec{E}_R(z,t) = \vec{E}_{0R} e^{i(-k_1 z - \omega t)} \hat{x}$$
$$\vec{B}_R(z,t) = \frac{\vec{E}_{0R}}{v_1} e^{i(-k_1 z - \omega t)} (-\hat{y})$$

Transmitted:
$$\vec{E}_T(z,t) = \vec{E}_{0T} e^{i(k_2 z - \omega t)} \hat{x}$$
$$\vec{B}_T(z,t) = \frac{\vec{E}_{0T}}{v_2} e^{i(k_2 z - \omega t)} \hat{y}$$

Reflection & Transmission at Normal Incidence



Boundary Conditions



Images show boundary conditions for case w/
no free charge or current at the boundary

$$\Delta \vec{E}_{\parallel} = 0$$

$$\Rightarrow \vec{E}_{0I} + \vec{E}_{0R} = \vec{E}_{0T}$$

$$\Delta \vec{H}_{\parallel} = 0$$

$$\Rightarrow \frac{1}{\mu_1} \left(\frac{\vec{E}_{0I}}{v_1} - \frac{\vec{E}_{0R}}{v_1} \right) = \frac{1}{\mu_2} \frac{\vec{E}_{0T}}{v_2}$$

Write $\beta = \frac{\mu_1 v_1}{\mu_2 v_2} = \frac{\mu_1 n_2}{\mu_2 n_1}$

Solution:

$$\vec{E}_{0R} = \frac{1-\beta}{1+\beta} \vec{E}_{0I}$$

$$\vec{E}_{0T} = \frac{2}{1+\beta} \vec{E}_{0I}$$

If $\mu_1 \sim \mu_2 \Rightarrow \beta = \frac{v_1}{v_2} = \frac{n_2}{n_1}$

$$\vec{E}_{0R} = \frac{v_2 - v_1}{v_2 + v_1} \vec{E}_{0I}, \quad \vec{E}_{0T} = \frac{2v_2}{v_1 + v_2} \vec{E}_{0I}$$

$v_2 > v_1$: $E_{0R} = \frac{v_2 - v_1}{v_2 + v_1} E_{0I}$, $E_{0T} = \frac{2v_2}{v_1 + v_2} E_{0I}$
 In phase reflection

$v_2 < v_1$: $E_{0R} = \frac{v_1 - v_2}{v_1 + v_2} E_{0I}$, $E_{0T} = \frac{2v_2}{v_1 + v_2} E_{0I}$
 Inverted reflection

Same as wave on a string!

In terms of n

$$E_{OR} = \left| \frac{n_1 - n_2}{n_1 + n_2} \right| E_{OI}$$

$$E_{OT} = \frac{2n_1}{n_1 + n_2} E_{OI}$$

Reflection & Transmission

$$I = \frac{1}{2} \epsilon E_0^2 v$$

$$R = \frac{I_R}{I_I} = \frac{E_{OR}^2}{E_{OI}^2} = \left(\frac{n_1 - n_2}{n_1 + n_2} \right)^2$$

If $\mu_1 = \mu_2$

$$\begin{aligned} T &= \frac{I_T}{I_I} = \frac{\epsilon_2 v_2 E_{OT}^2}{\epsilon_1 v_1 E_{OI}^2} \\ &= \frac{n_2^2}{n_1^2} \frac{n_1}{n_2} \left(\frac{2n_1}{n_1 + n_2} \right)^2 \\ &= \frac{4n_1 n_2}{(n_1 + n_2)^2} \quad \text{If } \mu_1 = \mu_2 \end{aligned}$$

$$\text{Note } R + T = \frac{n_1^2 - 2n_1 n_2 + n_2^2 + 4n_1 n_2}{(n_1 + n_2)^2}$$

$$= 1 \quad (\text{Always True})$$

Oblique Incidence

$$\vec{E}_I(\vec{r}, t) = \vec{E}_{0I} e^{i(\vec{k}_I \cdot \vec{r} - \omega t)} \hat{n}_I$$

$$\vec{B}_I(\vec{r}, t) = \frac{\vec{E}_{0I}}{v_1} e^{i(\vec{k}_I \cdot \vec{r} - \omega t)} \hat{k}_I \times \hat{n}_I$$

$$\vec{E}_R(\vec{r}, t) = \vec{E}_{0R} e^{i(\vec{k}_R \cdot \vec{r} - \omega t)} \hat{n}_R$$

$$\vec{B}_R(\vec{r}, t) = \frac{\vec{E}_{0R}}{v_1} e^{i(\vec{k}_R \cdot \vec{r} - \omega t)} \hat{k}_R \times \hat{n}_R$$

$$\vec{E}_T(\vec{r}, t) = \vec{E}_{0T} e^{i(\vec{k}_T \cdot \vec{r} - \omega t)} \hat{n}_T$$

$$\vec{B}_T(\vec{r}, t) = \frac{\vec{E}_{0T}}{v_2} e^{i(\vec{k}_T \cdot \vec{r} - \omega t)} \hat{k}_T \times \hat{n}_T$$

$$k_I v_1 = k_R v_1 = k_T v_2 = \omega$$

$$\Rightarrow k_I = k_R = \frac{v_2}{v_1} k_T = \frac{n_1}{n_2} k_T$$

$$\vec{E}_{I||}(z=0) + \vec{E}_{R||}(z=d) = \vec{E}_{T||}(z=0)$$

Must hold for all x, y, t

\Rightarrow exponential factors equal @ $z=0$

$$\Rightarrow \vec{k}_I \cdot \vec{r} = \vec{k}_R \cdot \vec{r} = \vec{k}_T \cdot \vec{r} \quad @ \quad z=0$$

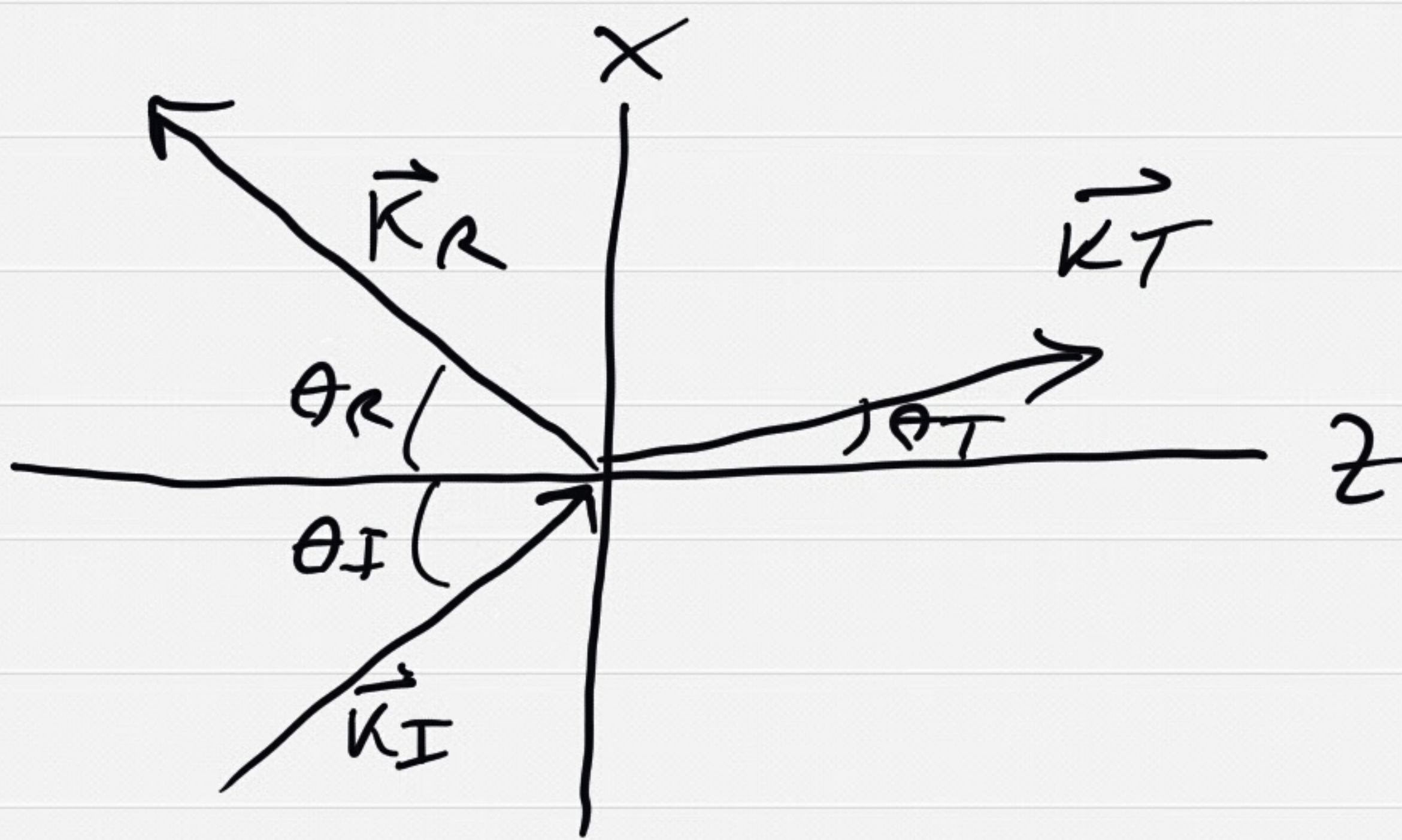
$$\begin{aligned} \Rightarrow k_{Ix} X + k_{Iy} Y &= k_{Rx} X + k_{Ry} Y \\ &= k_{Tx} X + k_{Ty} Y \end{aligned}$$

Must hold for all x, y

$$\Rightarrow k_{Ix} = k_{Rx} = k_{Tx}$$
$$k_{Iy} = k_{Ry} = k_{Ty}$$

This constraint is equivalent to saying that wave fronts have to line up with each other.

Since only k_z changes, all k vectors are in a plane. For convenience, we say this is $x-z$ plane



$$k_{Rx} = k_{Ix} \Rightarrow k_I \sin \theta_I = k_R \sin \theta_R$$

but $k_I = k_R \Rightarrow \boxed{\sin \theta_I = \sin \theta_R}$

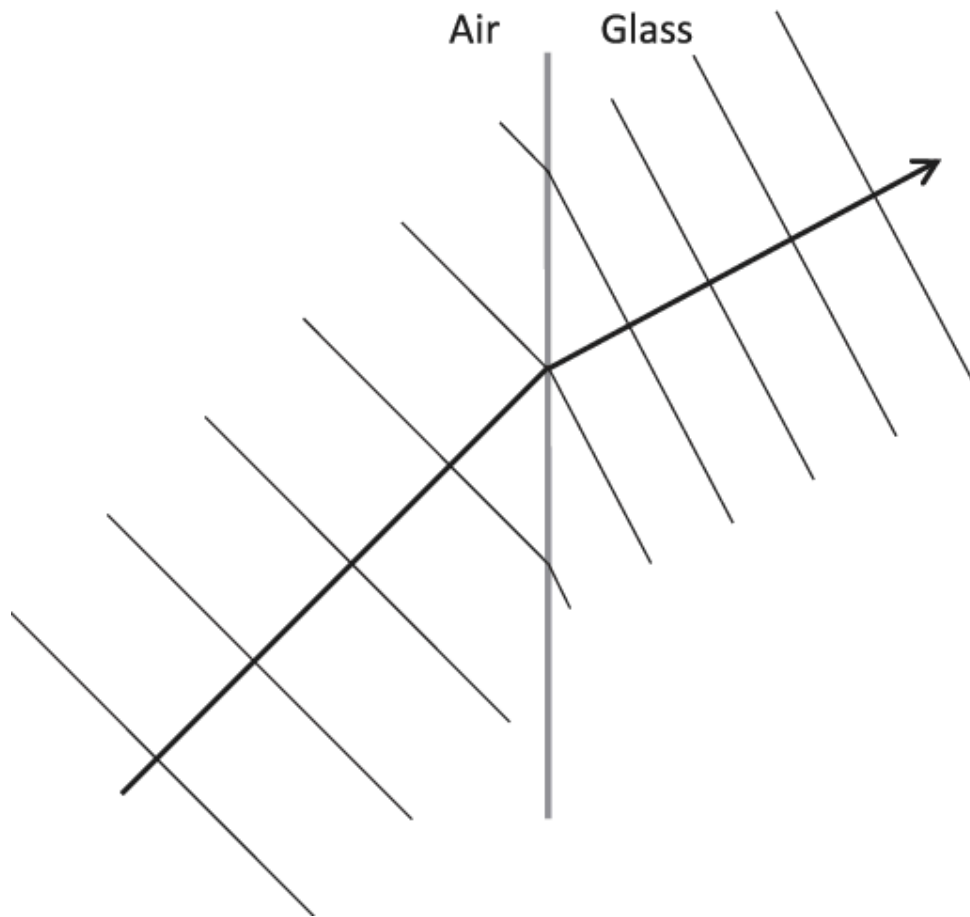
Equal Incidence/Reflection

$$k_{Ix} = k_{Tx} \Rightarrow k_I \sin \theta_I = k_T \sin \theta_T$$

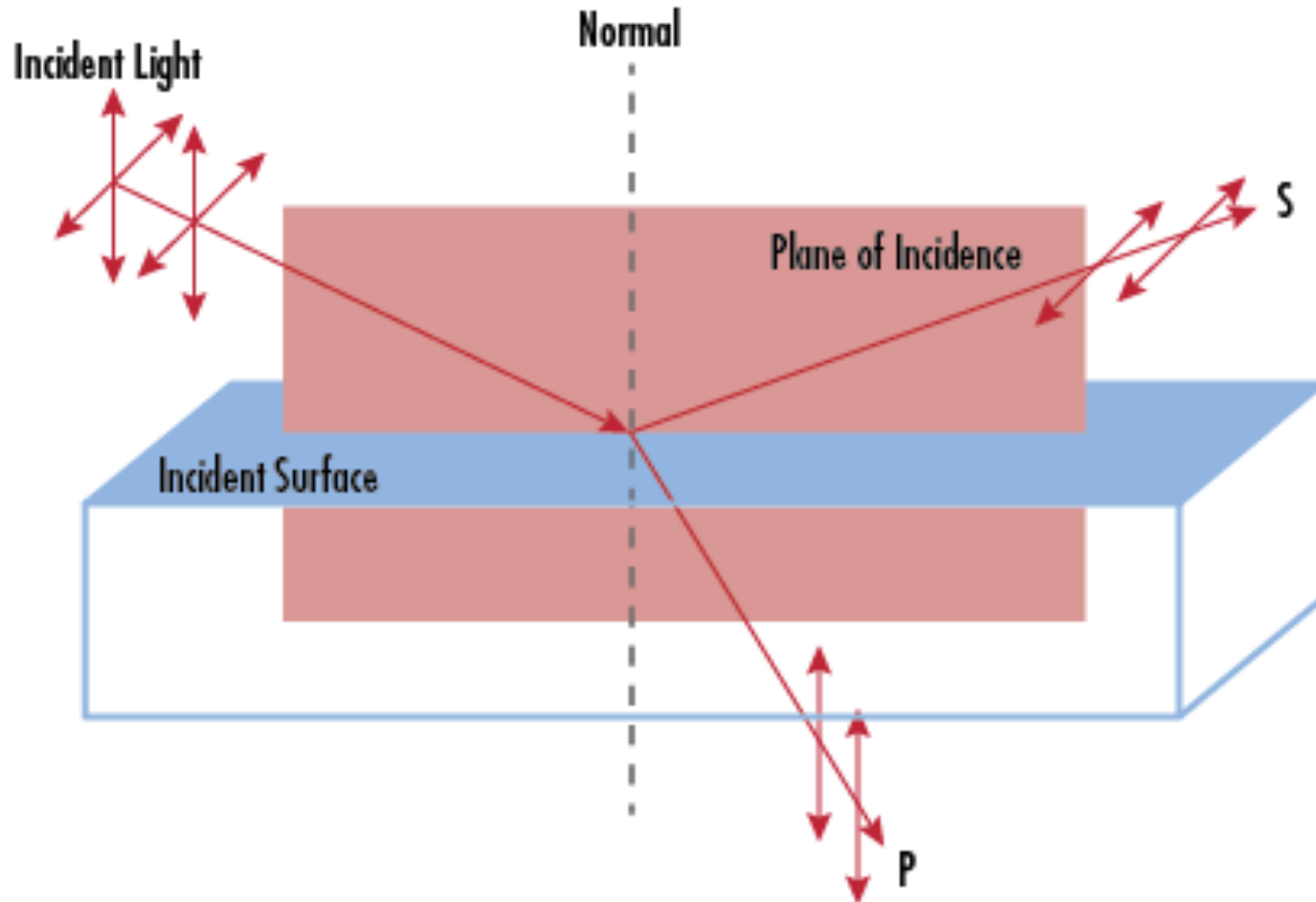
$$k_I = \frac{n_1}{n_2} k_T \Rightarrow \boxed{\frac{\sin \theta_T}{\sin \theta_I} = \frac{n_1}{n_2}}$$

Snell's Law

Snell's Law: Geometric Proof



S & P Polarization



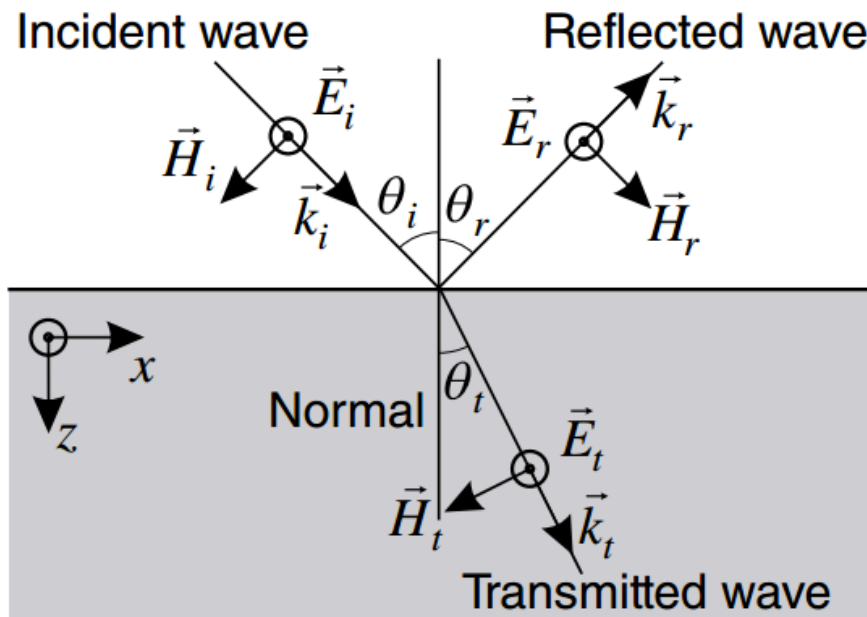
P-polarized (from the German parallel) light has an electric field polarized parallel to the plane of incidence, while s-polarized (from the German senkrecht) light is perpendicular to this plane.

Reflection & Transmission at Oblique Incidence

Out-of-Plane (S) Polarization

In-Plane (P) Polarization

1.



2.

